

ptic System Application

PARCEL
APP SEPTIC
YEAR
SCANNED
LAKE

915 Lake Ave, Detroit Lakes, MN 56501
Phone (218)-846-7314; Fax (218)-846-7266

| 1. PROPERTY DATA (as it appears on the tax statement, purchase agreement or deed) Parcel Number(s) of property where the system will be installed: |
|---|
| Is this a split of an existing property? Yes (No) (If yes and a parcel number has not yet been assigned, indicate the main parcel number from which the new parcel was split.) |
| Section 13 Township 139 Range 40 Township Name ERIE |
| Lake Name 10n - Shor Innol Lake Classification |
| Legal Description: Pt Sw/4 8E/4 Beg S Qh Cor Sec 13 E 570' N 260' w 260' w 250' w 250' |
| Project Address: 3 4450 190 ht s.t |
| 2. PROPERTY OWNER INFORMATION (as it appears on the tax statement, purchase agreement or deed) Owner's First Name 6 And & Break Owner's Last Name 6 And Am |
| Mailing Address 34450 190 th st City, State, Zip Detroit Linkey, mn 52501 |
| Phone Number |
| 3. DESIGNER/INSTALLER INFORMATION |
| Designer Name <u>Randy Anderson</u> Company Name <u>Anderson</u> On-sik License # 63 Y |
| Address P.O 1421 Detroit Lakes Phone Number 218 849 3072 |
| Installer Name Tason Niemi Company Name Magnum Construction License # 3225 |
| Address 43493 15014 St Frazec, mN 56544 Phone Number (218) 234-8076 RECEIVED |
| 4. SYSTEM DESIGN INFORMATION AUG 22 2014 |
| System Status What will new system serve? Check one |
| Vacant Lot-No existing system-new structure Replacement – structure removed and being rebuilt Failing –Replacement- cesspool/seepage pit or other Enlargement of system-Undersized Repairs Needed to existing Additional system on property Dwelling Resort/Commercial Commercial (Non-resort) Other – explain below |
| Design Flow 450 Gallons Per Day Number of Bedrooms 2 Sizing For 3 Depth of other wells within Garbage Disposal Yes No Dishwasher Yes No Lift station in House Yes No Grinder pump in House Yes No |
| Size of All Tanks to be installed gal Single Compartment Septic Tank gal Compartmented Tank Pit Privy gal Separate Lift Station Existing tank w/new Additional Tank Existing tank w/new Lift Station Existing Tank to be used Holding Tank with Privy |
| Total Number of tanks to be installed in this system (This # will be reported to MPCA at end of year.) |

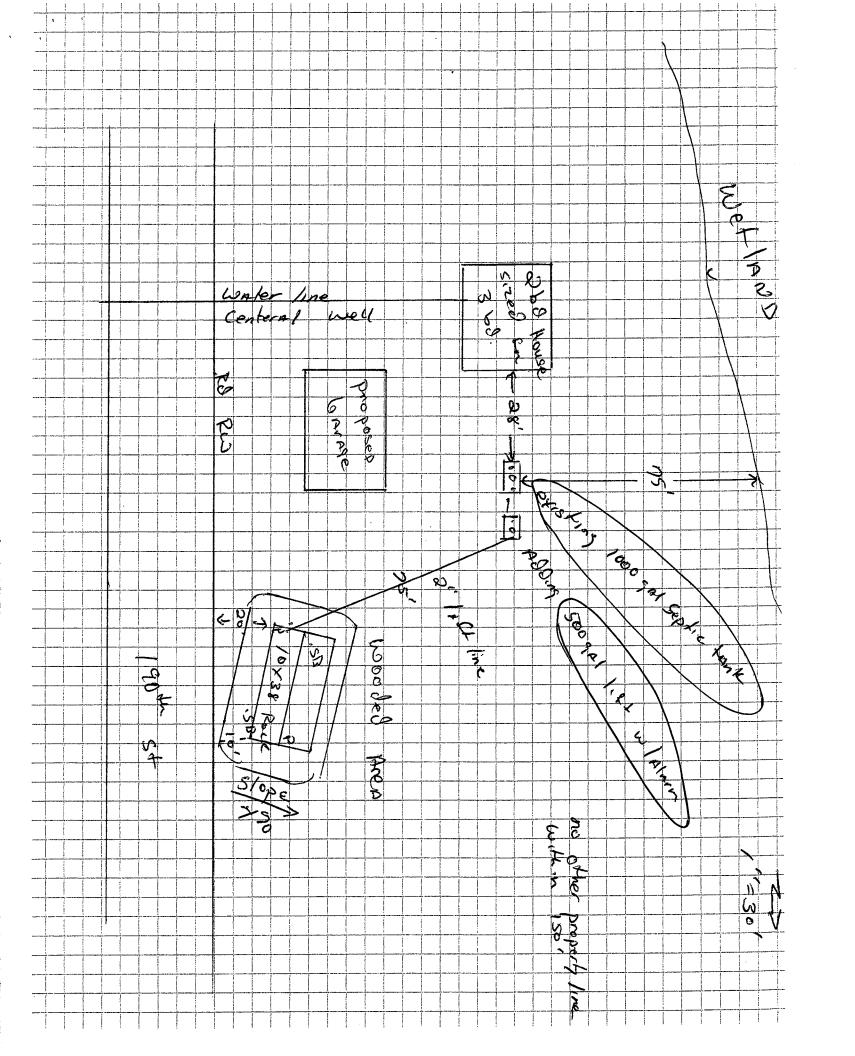
PARCEL SEPTIC

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| Type of Drain | field Fu | ıll Size of Drain | field Reduced/V | Warrantie | d size | Ĺ | YEAR | |] |
| | er Trench | sq ft | | sq ft | | chamber | | | |
| Rock T | ****** | sq ft | | sq ft | | | | | |
| Gravell | | sq ft | | sq ft | , | | | | |
| > Mound | | 760 sq ft | *** | X | | • | | | |
| Pressur | | sq ft | *** | | Alarm? | Yes | No | <u> </u> | |
| Seepag | | sq ft | *** | | | | | | |
| At-grad | | sq ft | *** | | Size of I | ift Pump <u>299</u> | gim @ 24 | hens | |
| Alterna | | sq ft | | Vorksheet | s Size of L | Lift Line | 2 m 0 24 | | |
| Perform | nance | · · | | | | | | | |
| | | | PROPOSED SE | | | | | | |
| | | | | DRAINFI | | | | | |
| Distance to W | | | 100+ | 100 F | - | | | | |
| Distance to Br | | | <u> </u> | 45 | . | | | | |
| Distance to Pr | | | <u>/00</u> _ | 100 | | | | | |
| Distance to O | | | | 1001 | | | | • | |
| Distance to Pr | | J 777-4 | 75 | 100+ | | | | | |
| Distance to W | etland/Protecte | a water | | 140 | | | | | |
| Daro Data | 23 | Soil Sizing I | Factor 1.6 | 7 | *1f cce ~ | ther than 02 a | ttach Perc Test I |) Nata | |
| Perc Rate | <u>~~</u> | son sixing i | cacioi / · · · | <u> </u> | .11 991 0 | unci man .03, a | maon reio 1681 l | Jula | |
| Soil Boringe | (three are requi | ired) | | | | | | | |
| Depth | Texture | Color | Structure | | Depth | Texture | Color | Structure | |
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| 24 | 10AM | 2.5444 | no Hed | | 97 x | loan | mo HHeel | Platy | J. |
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| Depth | Texture | Color | Structure | | Depth | Texture | Color | Structure | |
| Depui | Texture | | | - 44 | Берш | Toxidio | | Buractare | |
| 0-8 | loam | 10yR2/2 | pris | | | | | | |
| 8-23 | 10 Am | Blocket | 104R 4/4 | | | | | * | |
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| 5. REQUI | RED DOCUM | ENTS | • | | | | | | |
| ** ** | | | , , | 1 | | . 1 | V T V | utawa Anatha | ı |
| U of Mr | worksheets a | re required for | mounds, pressure b | oeas, seep | age beds, at-gra | ades or Type I | v or type v sy | stems. Are me | |
| required | worksheets atta | acned? | YesNo | | | | | | ı |
| | | | | | | | | | |
| 6. DESIGN | ER'S CERTIF | TED STATEM | ENT | | | | | | |
| ~ | 4 | | | | | | | | |
| I, KAN | OY /the | lesson | certify that I ha | ve compl | eted the precedi | ng design work | c in accordance v | vith all | |
| (Print Na | me of Designer | | | | • | - - | | | |
| | | | limited to Minneso | ota Chapte | er 7080 and the | Becker Count | y Individual Sev | wage Treatment | |
| System Ordin | | <u>-</u> - | | • | | | | | |
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| 1/v | lu | <u></u> | | | | | 7/21/ | 17 | |
| Signature of | Designer | | | | | Date | e | | |
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OSTP Design Summary Worksheet University of Minnesota



| Pr | roperty Owner/Client: Grant Graham | Project ID: | | v 12.08.06 | | | | |
|----|--|---------------------|--------------------|---------------|--|--|--|--|
| | Site Address: 34450 190th St. Detroit Lakes, MN 56501 | Date: | 7/21/14 |] | | | | |
| 1. | DESIGN FLOW AND TANKS | | | | | | | |
| | Design Flow: 450 Gallons Per Day (GPD) Note: The estimated design flow including a safety factor. For long to daily flow is recommended to | erm performance | , the average | | | | | |
| | Minimum Code Required Septic Tank Capacity: 1000 Gallons, in 1 | Tanks or Compar | tments | | | | | |
| | Recommended Septic Tank Capacity: 1000 Gallons, in 1 | Tanks or Compar | tments | | | | | |
| | Effluent Screen & Alarm? optional | J. 4 0. 00pa. | ••••• | | | | | |
| c. | Holding Tanks Only: | | | | | | | |
| | Number of Holding Tanks: Total Volume of Holding Tanks: | | Gallons | | | | | |
| | Type of High Level Alarm: | | | | | | | |
| D, | Pump Tank 1 Capacity: 500 Gallons Pump Tank 2 Capacity: | | Gallons | | | | | |
| 2. | SYSTEM TYPE | | | | | | | |
| ſ | Type of Soil Treatment and Dispersal Area* | | | | | | | |
| | ○ Trench ○ Bed ● Mound ○ At-Grade ○ Gravity Distribution ● Pressure Dist | ribution-Level (| O Pressure Distrib | ution-Unlevel | | | | |
| L | O Drip O Holding Tanl O Other | Elev = 100 |) ft | | | | | |
| Г | System Type Benchmark Lo | <u> </u> | | | | | | |
| ŀ | Type of Distri | L | | | | | | |
| | ☑ Type I ☐ Type III ☐ Type IV ☐ Type V | rock | | | | | | |
| 3, | SITE EVALUATION: | | | | | | | |
| Α. | Depth to Limiting Layer: 23 in 1.9 ft Elevation & Local | tion of Limiting La | ıyer: | ft | | | | |
| В. | Minimum required separation: 36 in 3.0 ft Location: | | | | | | | |
| В. | Measured Percent Land Slope : 4.0 % 0.0 Code Maximum | Depth of System: | -13 | in* | | | | |
| c. | Soil Texture: loam Perc Rate: 23 | MPI *if value is n | egative a mound i | s required | | | | |
| D. | Soil Hydraulic Loading Rate: 0.60 GPD/ft² E. Contour Loading Rate | 12.0 | Gal/ft | | | | | |
| 4. | DESIGN SUMMARY | | | | | | | |
| | Trench Design Summary | | | | | | | |
| | Dispersal Area ft ² Sidewall Depth in | Trencl | n Width | in | | | | |
| | Total Lineal Feet ft Number of Trenches Code | e Maximum Trencl | n Depth | in | | | | |
| | Des | igner's Max Trencl | n Depth | in | | | | |
| | Bed Design Summary | | | | | | | |
| | Absorption Area ft ² Media Below Pipe in C | ode Maximum Beo | d Depth | in | | | | |
| | Bed Width ft Bed Length ft | Designer's Max Bed | d Depth | in | | | | |
| | Mound Design Summary | | | | | | | |
| | Absorption Area 760 ft ² Bed Length 38 ft | Вес | d Width 10 |).0 ft | | | | |
| | Absorption Width 20.0 ft Clean Sand Lift 1.1 ft | Berm Width (slop | e 0-1%) | ft | | | | |
| | Upslope Berm Width 10.6 ft Downslope Berm Width 16.6 ft | Endslope Bern | n Width 1 | 3.9 ft | | | | |
| | Total System Length 65.9 ft Total System Width 37.2 ft | | | | | | | |



OSTP Design Summary Worksheet University OF MINNESOTA



| | At-Grade Design Summary | | | | | | | | |
|----|----------------------------|---------------|-----------|---------------------------|--------------|----------|--------------------------------|--------|-----|
| | Absorption Bed Width | | ft | Absorption Bed Length | | ft | System Height | | ft |
| | Absorption Bed Area | | ft² | Upslope Berm Width | | ft | Downslope Berm Width | | ft |
| | Endslope Berm Width | | ft | System Length | | ft | System Width | | ft |
| | | | | Level Pressure Dist | ribution Su | mmary | | | |
| | No. of Perforated Laterals | 3 | | Perforation Spacing | 3 | ft | Perforation Diameter | 1/4 | in |
| | Lateral Diameter | 2.00 | in | Supply Pipe Diameter | 2.00 | in | Minimum Dose Volume | 0 | gal |
| | Flow Rate | 29.0 | GPM | Total Head | 24 | ft | Maximum Dose Volume | 112.5 | gal |
| | Additional Info for Typ | e IV/Pretre | atment [| Design | | | | | |
| | A. Calculate the organic | loading usi | ng optio | n 1 or 2 | | | | | |
| | 1. Organic Loading = Pour | nds of BOD X | (Units | | | | | | |
| | lbs/day | х | | = | lbs BOD/da | y | | | |
| | 2. Organic Loading to Pre | treatment L | Init = De | sign Flow X Estimated B | OD in mg/L | . in the | effluent X 8.35 ÷ 1,000,000 | | |
| | gpd X | | | mg/L X 8.35 ÷ 1,000,00 | 0 = | | lbs BOD/day | | |
| | B. Type of Pretreatment l | Jnit Being In | stalled: | | | | | | |
| | C. Calculate Soil Treatme | nt System O | rganic Lo | ading: lbs. BOD/day ÷ B | ottom Area | = lbs/ | day/ft ² | | |
| | lbs/day | | | ft ² = | lbs/day/ft² | | | | |
| :o | mments/Special Design Co | nsiderations | i: | | | | | | |
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| | I hereby certify | that I have | complete | d this work in accordance | e with all a | pplicab | le ordinances, rules and laws. | | 크 |
| | • | | | 4 | | | | | |
| | Randy Andei | rson | | Mal | | | 634 07/ | /21/14 | |
| | (Designer | | _ | /// (Signature) | | | (License #) | Date) | _ |

Becker County, Minnesota

776B—Snellman-Sugarbush complex, 2 to 8 percent slopes

Map Unit Setting

Elevation: 800 to 2,000 feet

Mean annual precipitation: 20 to 28 inches Mean annual air temperature: 37 to 45 degrees F

Frost-free period: 90 to 150 days

Map Unit Composition

Snellman and similar soils: 60 percent Sugarbush and similar soils: 30 percent

Minor components: 10 percent

Description of Snellman

Setting

Landform: Hillslopes on moraines

Landform position (two-dimensional): Summit, shoulder, backslope

Down-slope shape: Linear Across-slope shape: Linear Parent material: Loamy glacial till

Typical profile

A - 0 to 3 inches: sandy loam
E - 3 to 12 inches: sandy loam
Bt - 12 to 32 inches: sandy clay loa

Bt - 12 to 32 inches: sandy clay loam Bk, C - 32 to 60 inches: sandy loam

Properties and qualities

Slope: 2 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 15 percent

Available water storage in profile: Moderate (about 8.5 inches)

Interpretive groups

Farmland classification: Farmland of statewide importance Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e

Line to de site On it Occasion D

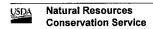
Hydrologic Soil Group: B

Description of Sugarbush

Setting

Landform: Hillslopes on moraines

Landform position (two-dimensional): Summit, shoulder, backslope



Down-slope shape: Linear Across-slope shape: Linear

Parent material: Loamy mantle over sandy and gravelly outwash

deposits

Typical profile

A - 0 to 3 inches: sandy loam
E - 3 to 17 inches: loamy sand
Bt - 17 to 28 inches: sandy loam

2C - 28 to 60 inches: gravelly coarse sand

Properties and qualities

Slope: 2 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (1.98

to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 15 percent Available water storage in profile: Low (about 4.6 inches)

Interpretive groups

Farmland classification: Farmland of statewide importance Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Minor Components

Balmlake

Percent of map unit: 2 percent

Wykeham

Percent of map unit: 2 percent

Eagleview

Percent of map unit: 2 percent

Two inlets

Percent of map unit: 2 percent

Egglake

Percent of map unit: 1 percent

Landform: Swales

Karlstad

Percent of map unit: 1 percent

Data Source Information

Soil Survey Area: Becker County, Minnesota Survey Area Data: Version 9, Dec 26, 2013



OSTP Mound Design Worksheet UNIVERSITY OF MINNESOTA

Minnesota Pollution Control Agency



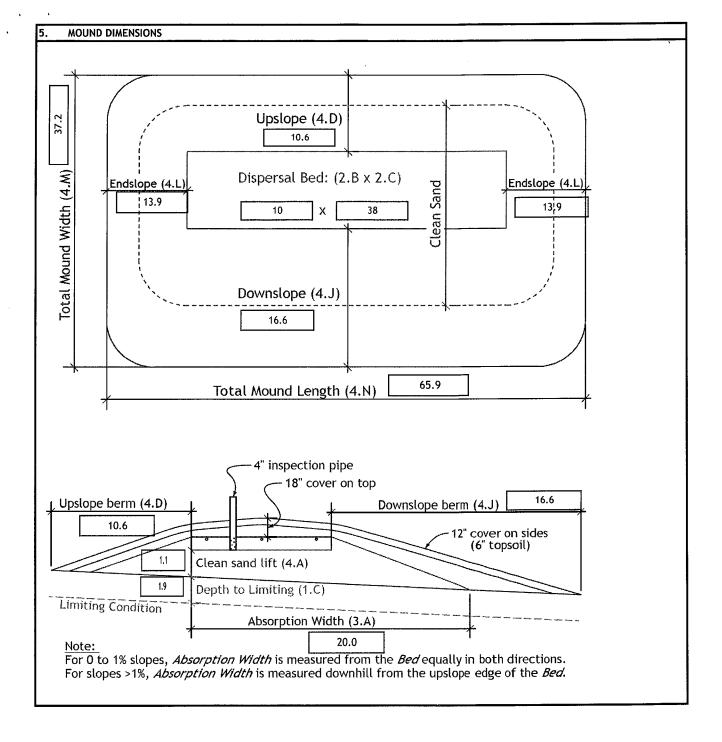
| SYSTEM SIZING: | Pro | oject ID: | | | | | v 12.08. |
|--|--|--|--|---|-----------------------------|---------------------------|--------------------------|
| A. Design Flow: | 450 | GPD | | TAE | LE IXa | 1 | |
| B. Soil Loading Rate: | 0.60 | GPD/ft ² | LOADING RATES | 100 mg | | 544445YP0000000000000 | C2330004/OCCCCC049N/C2G4 |
| C. Depth to Limiting Condition: | 1.9 | i ift | AND ABSORE | Treatmen | | RCOLATION Treatment Le | |
| D. Percent Land Slope: | 4.0 | 1 % | Percolation Rate | Absorption | Mound | Absorption | Mound |
| E. Design Media Loading Rate: | 1,2 | /^° ☐GPD/ft² | (MPI) | Area Loading Rate | Absorption Ratio | Area Loading Rate | Absorption Ratio |
| • | | | | (gpd/ft²) | | (gpd/ft ¹) | |
| F. Mound Absorption Ratio (Table IXa): | 2.00 | _ | <0.1 0.1 to 5 | 1.2 | 1 | 1.6 | 1 |
| G. Design Contour Loading Rate: | 12.0 | GPD/ft | 0.1 to 5 (fine sand | 0.6 | 2 | 1.0 | 1.6 |
| Table I MOUND CONTOUR LOADING RATES: | | | and loamy fine sand) 6 to 15 | 0.78 | 1.5 | 1 | 1.6 |
| Measured * Texture - derived | Contour | | 16 to 30 | 0.6 | 2 | 0.78 | 2 |
| Perc Rate OR mound absorption ratio | Loading Rate: | | 31 to 45 | 0.5 | 2.4 | 0.78 | 2 |
| ≤ 60mpi 1.0, 1.3, 2.0, 2.4, 2.6→ | ≤12 | | 46 to 60 | 0.45 | 2.6 | 0.6 | 2.6 |
| 2 dompt 1.0, 1.3, 2.0, 2.4, 2.6 | | | 61 to 120 | - | 5 | 0.3 | 5.3 |
| 61-120 mpi OR 5.0 | ≤12 | | >120 | | | • | - |
| DISPERSAL MEDIA SIZING | | | | | | | |
| A. Calculate Required Dispersal Bed Area: L | Design Flow (1. | A) ÷ Desigr | n Media Loading R | Rate (1.E) = | ft ² | | |
| 1 | | | = | | | | |
| | I ⊿5∩ | CBD · | 1 20 | DD /6+2 | | 375 | 2 |
| If a larger dispersal media area | 450 | GPD ÷ | 1.20 G | iPD/ft ² = | | 375 ft | 2 |
| If a larger dispersal media area is desired, enter size: | 450 380 | GPD ÷ | 1.20 G | iPD/ft ² = | | 375 ft | 2 |
| | 380 | ft² | | | L | | 2 |
| is desired, enter size: | 380 | ft² | gn Media Loading | g Rate (1.E) | = Bed Wid | | |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour I | 380 Loading Rate (1 | ft ² 1.G) ÷ Desi | gn Media Loading | ; | = Bed Wid | ith | |
| is desired, enter size: | 380 Loading Rate (1 12.0 al Bed Area (2.7 | ft ² 1.G) ÷ Desi ft ÷ [A) ÷ Bed W | gn Media Loading 1.2 g idth (2.B) = Bed | g Rate (1.E) pd/ft ² = Length | ≃ Bed Wid | dth 10 ft | |
| is desired, enter size: B. Calculate <i>Dispersal Bed Width: Contour I</i> | 380 Loading Rate (1 | ft ² 1.G) ÷ Desi | gn Media Loading | g Rate (1.E) pd/ft ² = Length | = Bed Wid | ith | |
| is desired, enter size: B. Calculate <i>Dispersal Bed Width: Contour I</i> | 380 Loading Rate (1 12.0 al Bed Area (2.7 | ft ² 1.G) ÷ Desi ft ÷ [A) ÷ Bed W | gn Media Loading 1.2 g idth (2.B) = Bed | g Rate (1.E) pd/ft ² = Length : = | ≃ Bed Wid | dth 10 ft | |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour I C. Calculate Dispersal Bed Length: Dispersal | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 | ft ² I.G) ÷ <i>Desi</i> ft ÷ [A) ÷ <i>Bed W</i> ft ² ÷ [| gn Media Loading 1.2 g idth (2.B) = Bed 10 ft | g Rate (1.E) pd/ft ² = Length : = | ≃ Bed Wid | dth 10 ft | |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour I C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng | ft ² I.G) ÷ Desi ft ÷ [A) ÷ Bed W ft ² ÷ [gth: | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft | g Rate (1.E) pd/ft ² = Length : = in ÷ | = Bed Wid | dth 10 ft | |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour II C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Contour II D. Enter Dispersal Media: | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng | ft ² I.G) ÷ Desi ft ÷ [A) ÷ Bed W ft ² ÷ [gth: | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock | g Rate (1.E) pd/ft ² = Length : = in ÷ | 38 12 = 12 = | dth 10 ft | ft |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour Bed. C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Center of the Center o | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng | ft ² I.G) ÷ Desi ft ÷ [A) ÷ Bed W ft ² ÷ [gth: | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock | g Rate (1.E) pd/ft ² = Length : = in ÷ (4.J) (Roun | 38 12 = 12 = | dth 10 ft | ft |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour Bed. C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Ced. F. If using a registered product, enter the Ced. G. Number of Components per Row = Bed Length: Dispersal | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng Component Wide Length (2.C) div | ft² I.G) ÷ Desi It ÷ [A) ÷ Bed W It² ÷ [gth: rided by Co | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock mponent Length componer (4.K) (Round up) | g Rate (1.E) pd/ft ² = Length : = in ÷ (4.J) (Roun | 38 12 = 12 = d up) | ft ft | ft |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour Bed. C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Ced. F. If using a registered product, enter the Ced. G. Number of Components per Row = Bed Length: Dispersal ft ÷ H. Number of Rows = Bed Width (2.B) divided Adjust Contour Loading Rate on Design Summer | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng Component Wide Length (2.C) div ft = ded by Compone mary page until t | ft² I.G) ÷ Desi It ÷ [A) ÷ Bed W It² ÷ [gth: rided by Co | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock imponent Length componer (4.K) (Round up) is a whole number. | g Rate (1.E) pd/ft ² = Length : = in ÷ (4.J) (Roun | 38 12 = 12 = d up) | ft ft | ft |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour Bed. C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Components per Row = Bed Length: Dispersal If the Length: Dispersal Media: F. If using a registered product, enter the Components per Row = Bed Length: Dispersal If the Length: Dispersal Media: If the | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng Component Wide ength (2.C) div ft = ded by Compone mary page until t | ft² I.G) ÷ Desi It ÷ [A) ÷ Bed W It² ÷ [gth: rided by Co ent Width this number | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock mponent Length componer (4.K) (Round up) is a whole number. rows | g Rate (1.E) pd/ft ² = Length : = in ÷ (4.J) (Roun ats/row | 38 12 = 12 = d up) | ft ft | ft |
| is desired, enter size: B. Calculate Dispersal Bed Width: Contour Bed. C. Calculate Dispersal Bed Length: Dispersal D. Enter Dispersal Media: E. If using a registered product, enter the Ced. F. If using a registered product, enter the Ced. G. Number of Components per Row = Bed Led. If the Ced. H. Number of Rows = Bed Width (2.B) divided Adjust Contour Loading Rate on Design Summers | 380 Loading Rate (1 12.0 al Bed Area (2.4 380 Component Leng Component Wide ength (2.C) div ft = ded by Compone mary page until t | ft² I.G) ÷ Desi It ÷ [A) ÷ Bed W It² ÷ [gth: rided by Co ent Width this number | gn Media Loading 1.2 g idth (2.B) = Bed 10 ft rock mponent Length componer (4.K) (Round up) is a whole number. rows | g Rate (1.E) pd/ft ² = Length : = in ÷ (4.J) (Roun ats/row | 38 12 = 12 = d up) | ft ft | ft |



| ABSORPTION AREA SIZING |
|--|
| Note: Mound setbacks are measured from the Absorption Area. |
| A. Calculate Absorption Width: Bed Width (2.B) X Mound Absorption Ratio (1.F) = Absorption Width |
| 10.0 ft X 2.0 = 20.0 ft |
| B. For slopes >1%, the Absorption Width is measured downhill from the upslope edge of the Bed. |
| Calculate Downslope Absorption Width: Absorption Width (3.A) - Bed Width (2.B) = ft |
| 20.0 ft - 10.0 ft = 10.0 ft |
| MOUND SIZING |
| A. Calculate Clean Sand Lift: 3 feet minus Depth to Limiting Condition (1.C) = Clean Sand Lift (1 ft minimum) |
| 3.0 ft - 1.9 ft = 1.1 ft Design Sand Lift (optional): |
| B. Calculate Upslope Height: Clean Sand Lift (4.A) + media depth + cover (1 ft.) = Upslope Height |
| 1.1 ft + 1.0 ft + 1.0 ft = 3.1 ft |
| D-34: Slope Multiplier Table Land Slope % 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 |
| Upslope 3:1 3.00 2.91 2.83 2.75 2.68 2.61 2.54 2.48 2.42 2.36 2.31 2.26 2.21 2.17 2.13 2.09 2.06 2.03 2.00 1.97 1.95 1.93 1.91 1.89 1.87 1.85 |
| Berm Ratio 4:1 4.00 3.85 3.70 3.57 3.45 3.33 3.23 3.12 3.03 2.94 2.86 2.78 2.70 2.62 2.55 2.48 2.41 2.35 2.29 2.23 2.18 2.13 2.08 2.03 1.98 1.93 |
| Land Slope % 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 |
| Downslope 3:1 3.00 3.09 3.19 3.30 3.41 3.53 3.66 3.80 3.95 4.11 4.29 4.48 4.69 4.95 5.24 5.55 5.88 6.24 6.63 7.04 7.47 7.93 8.42 8.93 9.46 10.02 |
| Berm Ratio 4:1 4.00 4:17 4:35 4:54 4:76 5:00 5:26 5:56 5:88 6:25 6:67 7:14 7:69 8:29 8:32 9:57 10:24 10:94 11:67 12:42 13:19 13:99 14:82 15:67 16:54 17:44 |
| C. Select Upslope Berm Multiplier (based on land slope): 3.45 (figure D-34) |
| D. Calculate Upslope Berm Width: Multiplier (4.C) X Upslope Mound Height (4.B) = Upslope Berm Width |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ |
| E. Calculate Drop in Elevation Under Bed: Bed Width (2.B) \times Land Slope (1.D) \div 100 = Drop (ft) 10.0 ft \times 4.0 $\%$ \div 100 = 0.40 ft |
| F. Calculate Downslope Mound Height: Upslope Height (4.B) + Drop in Elevation (4.E) = Downslope Height |
| 3.1 ft + $\begin{pmatrix} 0.40 \\ ft = \end{pmatrix}$ ft |
| G. Select Downslope Berm Multiplier (based on land slope): 4.76 (figure D-34) |
| H. Calculate Downslope Berm Width: Multiplier (4.G) X Downslope Height (4.F) = Downslope Berm Width |
| 4.76 x 3.5 ft = 16.6 ft |
| I. Calculate Minimum Berm to Cover Absorption Area: Downslope Absorption Width (3.B or 3.C) + 4 ft. = ft |
| $\begin{array}{ c c c c c c }\hline 10.0 & ft + \boxed{} & 4 & ft = \boxed{} & 14.0 & ft \\ \hline \end{array}$ |
| J. Design Downslope Berm = greater of 4H and 4I: 16.6 ft |
| K. Select Endslope Berm Multiplier: 4.00 (usually 3.0 or 4.0) |
| L. Calculate Endslope Berm (4.K) X Downslope Mound Height (4.F) = Endslope Berm Width |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ |
| M. Calculate Mound Width: Upslope Berm Width (4.D) + Bed Width (2.B) + Downslope Berm Width (4.J) = ft |
| 10.6 ft + 10.0 ft + 16.6 ft = 37.2 ft |
| N. Calculate Mound Length: Endslope Berm Width $(4.L)$ + Bed Length $(2.C)$ + Endslope Berm Width $(4.L)$ = ft 13.9 ft + 38.0 ft + 13.9 ft = 65.9 ft |
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| Comments: |
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OSTP Mound Materials Worksheet University OF MINNESOTA



| A. Calculate Bed (rock) Volume: Bed Length (2.C) X Bed Width (2.B) X Depth = Volume (ft²) 38.0 ft X 10.0 ft X 1.0 = 380.0 ft² Divide ft² by 27 ft²/yd³ to calculate cubic yards: 380.0 ft³ + 27 = 14.1 yd³ Add 20% for constructability: 14.1 yd³ X 1.2 = 16.9 yd³ B. Calculate Clean Sand Volume: Volume Under Rock bed: Average Sand Depth × Media Width × Media Length = cubic feet 1.3 ft X 10.0 ft X 38.0 ft = 487.7 ft³ For a Mound on a slope from 0-1% Volume from Length = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Length) [|
|---|
| Divide ft³ by 27 ft³/yd³ to calculate cubic yards: 380.0 |
| Second Structability: Seco |
| B. Calculate Clean Sand Volume: Volume Under Rock bed: Average Sand Depth × Media Width × Media Length = cubic feet 1.3 ft × 10.0 ft × 38.0 ft = 487.7 ft ³ For a Mound on a slope from 0-1% Volume from Length = ((Upslope Mound Height - 1) × Absorption Width Beyond Bed × Media Bed Length) ft - 1) x |
| B. Calculate Clean Sand Volume: Volume Under Rock bed: Average Sand Depth x Media Width x Media Length = cubic feet 1.3 ft X 10.0 ft X 38.0 ft = 487.7 ft³ For a Mound on a slope from 0-1% Volume from Length = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Length) Total Clean Sand Volume: Volume from Length + Volume from Width + Volume Under Media ft³ + ft³ + ft³ = ft³ For a Mound on a slope greater than 1% Upslope Volume: ((Upslope Mound Height - 1) X 3 X Bed Length) + 2 = cubic feet ((3.1 ft - 1) X 3.0 ft X 38.0) + 2 = 118.8 ft³ Endslope Volume: ((Downslope Height - 1) X 3 X Media Width = cubic feet ((3.5 ft - 1) X 10.0 ft X 38.0) + 2 = 471.8 ft³ Endslope Volume: ((Downslope Mound Height - 1) X 3 X Media Width = cubic feet ((3.5 ft - 1) X 3.0 ft X 10.0 ft = 74.5 ft³ |
| B. Calculate Clean Sand Volume: Volume Under Rock bed: Average Sand Depth x Media Width x Media Length = cubic feet 1.3 ft X 10.0 ft X 38.0 ft = 487.7 ft³ For a Mound on a slope from 0-1% Volume from Length = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Length) ft - 1) X X ft = Volume from Width = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Width) ft - 1) X X ft = Total Clean Sand Volume: Volume from Length + Volume from Width + Volume Under Media ft³ + ft³ + ft³ + ft³ = For a Mound on a slope greater than 1% Upslope Volume: ((Upslope Mound Height - 1) X 3 X Bed Length) + 2 = cubic feet ((3.1 ft - 1) X 3.0 ft X 38.0) + 2 = 118.8 ft³ Downslope Volume: ((Downslope Height - 1) x Downslope Absorption Width x Media Length) + 2 = cubic feet ((3.5 ft - 1) X 3.0 ft X 38.0) + 2 = 471.8 ft³ Endslope Volume: ((Downslope Mound Height - 1) x 3 x Media Width = cubic feet ((3.5 ft - 1) X 3.0 ft X 10.0 ft X 74.5 ft³ |
| Volume Under Rock bed: Average Sand Depth \times Media Width \times Media Length = cubic feet 1.3 ft \times 10.0 ft \times 38.0 ft = 487.7 ft ³ For a Mound on a slope from 0-1% Volume from Length = ((Upslope Mound Height - 1) \times Absorption Width Beyond Bed \times Media Bed Length) [ft - 1) \times |
| 1.3 ft x 10.0 ft x 38.0 ft = 487.7 ft |
| Volume from Length = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Length) ft -1) X |
| Volume from Length = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Length) ft -1) X |
| Volume from Width = ((Upslope Mound Height - 1) X Absorption Width Beyond Bed X Media Bed Width) ft - 1) X |
| Total Clean Sand Volume: Volume from Length + Volume from Width + Volume Under Media |
| Total Clean Sand Volume: Volume from Length + Volume from Width + Volume Under Media $ ft^3 + ft^3 + ft^3 + ft^3 = ft^3 $ For a Mound on a slope greater than 1% Upslope Volume: ((Upslope Mound Height - 1) × 3 × Bed Length) + 2 = cubic feet $ ((3.1 ft - 1) $ |
| For a Mound on a slope greater than 1% Upslope Volume: ((Upslope Mound Height - 1) \times 3 \times Bed Length) + 2 = cubic feet ((\(\begin{align*} 3.1 & \text{ft - 1} \\ X & 3.0 \text{ft } \\ \end{align*} \) Downslope Volume: ((Downslope Height - 1) \times Downslope Absorption Width \times Media Length) + 2 = cubic feet ((\(\begin{align*} 3.5 & \text{ft - 1} \\ X & 10.0 & \text{ft } \\ \end{align*} \) Endslope Volume: ((Downslope Mound Height - 1) \times 3 \times Media Width = cubic feet ((\(\begin{align*} 3.5 & \text{ft - 1} \) \text{30.0} \\ \end{align*} \) For a Mound on a slope greater than 1% 18.8 \text{ft}^3 18.8 \text{or} \) For a Mound on a slope greater than 1% 18.8 \text{of t} \) 18.8 \text{of t} \) For a Mound on a slope greater than 1% 18.8 \text{of t} \) 18.8 \text{of t} \) 18.8 \text{of t} \) For a Mound on a slope greater than 1% 18.8 \text{of t} \) 18.8 \text{of t} \text{of t} \) 18.8 \text{of t} o |
| For a Mound on a slope greater than 1% Upslope Volume: ((Upslope Mound Height - 1) × 3 × Bed Length) + 2 = cubic feet ((|
| Upslope Volume: ((Upslope Mound Height - 1) \times 3 \times Bed Length) + 2 = cubic feet ((\(\begin{array}{cccccccccccccccccccccccccccccccccccc |
| Downslope Volume: ((Downslope Height - 1) \times Downslope Absorption Width \times Media Length) + 2 = cubic feet ((\begin{array}{cccccccccccccccccccccccccccccccccccc |
| Downslope Volume: ((Downslope Height - 1) \times Downslope Absorption Width \times Media Length) + 2 = cubic feet ((3.5 |
| ((|
| Endstope Volume: (Downstope Mound Height - 1) \times 3 \times Media Width = cubic feet (3.5 ft - 1) \times 3.0 ft \times 10.0 ft = 74.5 ft ³ |
| (3.5 ft - 1) X 3.0 ft X 10.0 ft = 74.5 ft ³ |
| |
| Total Clean Sand Volume: Upslope Volume + Downslope Volume + Endslope Volume + Volume Under Media |
| |
| 118.8 $ft^3 + 471.8 	 ft^3 + 74.5 	 ft^3 + 487.7 	 ft^3 = 1152.8 	 ft^3$ |
| |
| Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: |
| Add 20% for constructability: |
| C. Calculate Sandy Berm Volume: |
| Total Berm Volume (approx): ((Avg. Mound Height · 0.5 ft topsoil) × Mound Width × Mound Length) ÷ 2 = cubic feet |
| (3.3 . 0.5)ft X 37.2 ft X 65.9) \div 2 = 3411.6 ft ³ |
| Total Mound Volume - Clean Sand volume -Rock Volume = cubic feet |
| 3411.6 ft^3 - 1152.8 ft^3 - 380.0 ft^3 = 1878.8 ft^3 |
| Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: 1878.8 ft ³ ÷ 27 = 69.6 yd ³ |
| Add 20% for constructability: $69.6 	 yd^3 \times 1.2 = 83.5 	 yd^3$ |
| |
| D. Calculate Topsoil Material Volume: Total Mound Width X Total Mound Length X .5 ft |
| 37.2 ft X 65.9 ft X 0.5 ft = 1225.7 ft ³ |
| Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: 1225.7 ft ³ ÷ 27 = 45.4 yd ³ |
| Add 20% for constructability: $45.4 	 yd^3 \times 1.2 = 54.5 	 yd^3$ |



Minnesota Pollution Control Agency

OSTP Pressure Distribution Design Worksheet





| | itioi Agency | | | | Proje | ct ID: | | | | | | v 12.08.06 |
|--|---|------------|------------|-------------|----------------|------------|-----------------------|------------------|------------|----------------|----------------|------------|
| 1. | Media Bed Width: | | | | | 10 | ft | | | | | |
| 2. | 2. Minimum Number of Laterals in system/zone = [(Media Bed Width (Line1) - 4) ÷ 3] + 1 round up to the neareast whole number + 1. | | | | | | | | | | | |
| | | (10 | | -4)+ | | 3 | \neg | · | | | | |
| | | | | | | | | | | | | |
| 3. | 3. Designer Selected Number of Laterals: Cannot be less than line 2 (accept in at-grades) Insulated access box | | | | | | | | | | | |
| 4. | | | | | | | | V | | | | |
| 5. | Geotextile | | | | | | 12* | | | | | |
| 6. | 6. Length of Laterals = Media Bed Length - 2 Feet. | | | | | | | | | | | |
| | 38 - | 2ft | = | 36 | ft | Perforatio | n can not be closer | then 1 fo | | Perforation sp | acing: 2° to 3 | |
| 7. | Determine the <i>Num</i> round down to the r | | | - | — Divide th | e Length o | f Laterals (Line 6) I | oy the <i>Pe</i> | rforation | Spacing (| Line 4) ar | nd |
| | Number of Perforat | ion Space | s = | 36 | ft | ÷ | 3 ft | = | 12 | Spaces | | |
| 8. Number of Perforations per Lateral is equal to 1.0 plus the Number of Perforation Spaces (Line 7). Check table below to verify the number of perforations per lateral guarantees less than a 10% discharge variation. The value is double with a center manifold. | | | | | | | | | | | | |
| Perforations Per Lateral = 12 Spaces + 1 = 13 Perfs. Per Lateral | | | | | | | | | | | | |
| Maximum Number of Perforations Per Lateral to Guarantee < 10% Discharge Variation | | | | | | | | | | | | |
| 1/4 Inch Perforations 7/32 Inch Perforations | | | | | | | | | | | | |
| Perforation Spacing (Feet) Pipe Diameter (Inches) Perforation Spacing Perforation Spacing Pipe Diameter (Inches) | | | | nches) | | | | | | | | |
| FEIL | y across spacing (reec) | 1 | 114 | 11/2 | 2 | 3 | (Feet) | - | 114 | 115 | 2 | 3 |
| 1.05 | 2 | 10 | 13 | 18 | 30 | 60 | 2 | 11 | 16 | 21 | 34 | 68 |
| ····· | 21/1 | 8 | 12 | 16 | 28 | 54 | 21/1 | 10 | 14 | 20 | 32 | 64 |
| | 3 | 8 | 12 | 16 | 25 | 52 | 3 | 9 | 14 | 19 | 30 | 60 |
| | | 3/16 Inch | Perforatio | ns | | | | 1/8 1 | nch Perfor | | | |
| Porfe | oration Spacing (Feet) | | Pipe C |)iameter (I | nches) | | Perforation Spacing | | Pipe [|)iameter (li | | |
| | | 1 | 114 | 11/2 | 2 | 3 | (Feet) | 1 | 114 | 11/2 | 2 | 3 |
| | 2 | 12 | 18 | 26 | 46 | 87 | 2 | 21 | 33 | 44 | 74 | 149 |
| 7250,07696245 | 21/2 | 12 | 17 | 24 | 40 | 80 | 21/1 | 20 | 30 | 41 | 69 | 135 |
| | 3 | 12 | 16 | 22 | 37 | 75 | 3 | 20 | 29 | 38 | 64 | 128 |
| 9. Total Number of Perforations equals the Number of Perforations per Lateral (Line 8) multiplied by the Number of Perforated Laterals (Line 3). | | | | | | | | | | | | |
| | 13 Perf. | Per Later | al X | | 3 | Number of | f Perf. Laterals | = | 39 | Total Nu | umber of I | Perf. |
| 10. | Select Type of Mani | ifold Conn | ection (E | nd or Cen | ter): | ☑ End | Center Center | | | | | |
| 11. | 11. Select Lateral Diameter (See Table): 2.00 in | | | | | | | | | | | |



OSTP Pressure Distribution Design Worksheet

| University |
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| OF MINNESOTA |

| 12. Calculate the Square Feet per Perforation. Recommended value is 4-11 ft ² per perforation. Does not apply to At-Grades a. Bed Area = Bed Width (ft) X Bed Length (ft) 10 | 16 | meter /32 |
|---|---|--|
| a. Bed Area = Bed Width (ft) X Bed Length (ft) 10 ft | 1/8 3/16 7, 0.18 0.41 0. 0.22 0.51 0. 0.26 0.59 0. 0.29 0.65 0. 0.32 0.72 0. 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to reperforations Dwellings with 1/8 inch perferotions Table II Volume of Liquiper Pipe Pipe Pipe Liquiper Pipe Cinches) (Gall 1 0.00 1.25 0.00 | / ₁₂ 1/ ₄ .56 0.76 .69 0.9 .80 1.04 .89 1.13 .98 1.28 .13 1.47 .26 1.65 .174 inch .275 with 3/16 .28 .28 |
| b. Square Foot per Perforation = Bed Area divided by the Total Number of Perforations (Line 9). 380 ft² ÷ 39 perforations = 9.7 ft²/perforations 3. Select Minimum Average Head: 1.0 ft 4. Select Perforation Discharge (GPM) based on Table: 0.74 GPM per Perforation 5. Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 8. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 16 | 1.56 0.74 1.69 0.9 1.80 1.98 1.28 1.13 1.47 1.26 1.65 1/4 inch forations STS with 3/16 is STS with 1/8 ir id in id in luid Foot lons) |
| b. Square Foot per Perforation = Bed Area divided by the Total Number of Perforations (Line 9). 380 ft² ÷ 39 perforations = 9.7 ft²/perforations 3. Select Minimum Average Head: 1.0 ft 4. Select Perforation Discharge (GPM) based on Table: 0.74 GPM per Perforation 5. Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 8. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.22 0.51 0. 0.26 0.59 0. 0.29 0.65 0. 0.32 0.72 0. 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to perforations Dwellings with 1/8 inch perforations Other establishments and MS inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquippe Pipe Pipe Liquippe Pipe Cinches) (Gall 1 0.00 1.25 0.00 | .69 0.9 .80 1.04 .89 1.17 .98 1.28 .13 1.47 .26 1.65 1/4 inch forations STS with 3/16 s STS with 1/8 ir id in uid Foot lons) |
| 380 ft² ÷ 39 perforations = 9.7 ft²/perforations 3. Select Minimum Average Head: 1.0 ft 4. Select Perforation Discharge (GPM) based on Table: 0.74 GPM per Perforation 5. Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 8. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.26 0.59 0. 0.29 0.65 0. 0.32 0.72 0. 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to reperforations Dwellings with 1/8 inch perforations Other establishments and MS inch to 1/4 inch perforations Table II Volume of Liquiple Pipe Pipe Pipe Liquiple Pipe Cinches) (Gall 1 0.00 1.25 0.0 | 1.94 1.98 1.28 1.13 1.47 1.26 1.65 1/4 inch 1.98 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.7 |
| 3. Select Minimum Average Head: 1.0 ft 4. Select Perforation Discharge (GPM) based on Table: 0.74 GPM per Perforation 5. Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 8. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.29 0.65 0. 0.32 0.72 0. 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to reperforations Dwellings with 1/8 inch perforations Other establishments and MS inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquit Pipe Pipe Liquit Pipe Pipe Liquit Oidents (Gall 1.25 0.00 1.25 0.01 | .89 1.17 .98 1.28 .13 1.47 .26 1.65 1/4 inch forations STS with 3/16 s STS with 1/8 in id in id in Foot lons) |
| 3. Select Minimum Average Head: 1.0 ft 4. Select Perforation Discharge (GPM) based on Table: 5. Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 8. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.32 0.72 0.30 1. 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to perforations Dwellings with 1/8 inch performents and MS inch to 1/4 inch perforations Table II Volume of Liquit Pipe Pipe Liquit Pipe Diameter (inches) (Gall 1.25 0.00 1.25 0.01 | 98 1.28 .13 1.47 .26 1.65 1/4 inch forations STS with 3/16 s STS with 1/8 in id in uid Foot Jons) |
| 4. Select Perforation Discharge (GPM) based on Table: Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 5. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.37 0.83 1. 0.41 0.93 1. Dwellings with 3/16 inch to operforations Dwellings with 1/8 inch performents and MS inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquit Pipe Pipe Liquit Pipe Diameter (inches) (GaII 0.00 1.25 0.00 1.5 0.1 | .13 |
| 4. Select Perforation Discharge (GPM) based on Table: Determine required Flow Rate by multiplying the Total Number of Perforations by the Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 5. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | 0.41 0.93 1. Dwellings with 3/16 inch to perforations Dwellings with 1/8 inch perforations Dwellings with 1/8 inch perforations Other establishments and MS perforations Table II Volume of Liquit Pipe Pipe Liquit Pipe Diameter (Gall 1 0.00 1.25 0.00 1.5 0.1 | .26 1.65 1/4 inch forations STS with 3/16 s STS with 1/8 in id in uid Foot lons) |
| Perforation Discharge. 39 Perfs X 0.74 GPM per Perforation = 29 GPM 5. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 X 36 ft X 0.170 gal/ft = 18.4 Gallons 3. Minimum Dose = Volume of Distribution Piping (Line 17) X 4 18.4 gals X 4 = 73.4 Gallons | perforations Dwellings with 1/8 inch performents and MS inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquit Pipe Pipe Liquit Pipe Diameter (Gall III) 1 0.0 1.25 0.0 1.5 0.1 | forations STS with 3/16 s STS with 1/8 in id in juid Foot Jons) |
| 39 Perfs X 0.74 GPM per Perforation = 29 GPM 5. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 7. Volume of Distribution Piping = = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 | Other establishments and MS inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquin Pipe Pipe Pipe Liquin Pipe Diameter (inches) (Gall 1 0.0 1.25 0.0 1.5 0.1 | STS with 3/16 s STS with 1/8 in id in juid Foot lons) |
| 39 Perfs X 0.74 GPM per Perforation = 29 GPM 6. Volume of Liquid Per Foot of Distribution Piping (Table II): 0.170 Gallons/ft 5 feet 7. Volume of Distribution Piping = = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 | inch to 1/4 inch perforations Other establishments and MS perforations Table II Volume of Liquid Pipe Pipe Liquid Diameter (inches) (GaII 1 0.00 1.25 0.00 1.5 0.1 | s STS with 1/8 in id in juid Foot lons) |
| 7. Volume of Distribution Piping = = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 | Perforations Table II Volume of Liquical Pipe Pipe Liquical Liquical Pipe (Gall 1 0.0 1.25 0.0 1.5 0.1 | id in uid Foot lons) |
| = [Number of Perforated Laterals (Line 3) X Length of Laterals (Line 6) X (Volume of Liquid Per Foot of Distribution Piping (Line 16)] 3 | Volume of Liquippe Pipe Liquippe Diameter (inches) (Gall 1 0.0 1.25 0.0 1.5 0.1 | uid Foot Ions) |
| alternate location of pipe from pump | 3 0.3 4 0.6 | 110 170 380 |





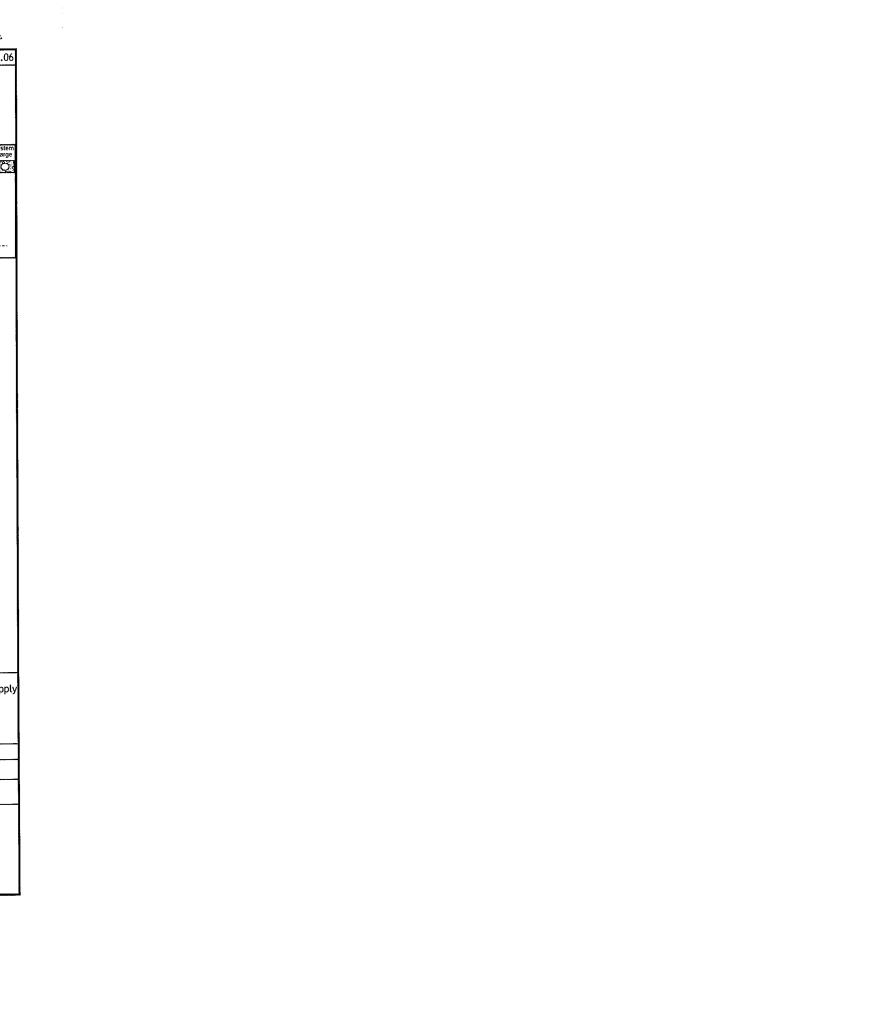


OSTP Basic Pump Selection Design Worksheet

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| NNESOTA | |

| I. PUMP CAPACITY | Project ID: | | | v 12.08.0 |
|---|---|---------------------------------------|---|--|
| Pumping to Gravity or Pressure Distribution: | ○ Gravity ● Pressure | Selection req | uired | |
| 1. If pumping to gravity enter the gallon per minute of | of the pump: | GPM (10 | 45 gpm) | |
| 2. If pumping to a pressurized distribution system: | 29. | 0 GPM | | |
| (Line 11 of Pressure Distribution) | | | | Soil treatment system & point of discharge |
| 2. HEAD REQUIREMENTS | | | | & point of discharge |
| A. Elevation Difference 17 ft | | | Supply line length | |
| between pump and point of discharge: | Inlet p | ipe | Elevation or | |
| | l Name | | difference | |
| B. Distribution Head Loss: 5 ft | | 1度 英[[]] | | |
| C. Additional Head Loss: | ue to special equipment, etc.) | | | |
| | | Table I.Friction | Loss in Plastic Pipe pe | r 100ft |
| Distribution Head Lo | 55 | Flow Rate | Pipe Diameter (inch | |
| Gravity Distribution = Oft | | (GPM) | 1 1.25 1.5 | 2 |
| Pressure Distribution based on Minimur | n Average Head | 10 | 9.1 3.1 1.3 | 0.3 |
| Value on Pressure Distribution Workshe | et: | 12 | 12.8 4.3 1.8 | 0.4 |
| Minimum Average Head Distrib | ution Head Loss | 14 | 17.0 5.7 2.4 | 0.6 |
| 1ft | 5ft | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 21.8 7.3 3.0 | 0.7 |
| 2ft | 6ft | 18 | 9.1 3.8 | 0.9 |
| 5ft | 10ft | 20 | 11.1 4.6 | 1.1 |
| | | 25 | 16.8 6.9 | 1.7 |
| . 1. Supply Pipe Diameter: 2.0 in | | 30 | 23.5 9.7 | 2.4 |
| | | 35 | 12.9 | 3.2 |
| 2. Supply Pipe Length: 80 ft | | 40 | 16.5 | 4.1 |
| . Friction Loss in Plastic Pipe per 100ft from Table I: | | 45 | 20.5 | 5.0 |
| <u> </u> | | 50 | | 6.1 |
| Friction Loss = 2.23 ft per 100ft of | of pipe | 55 | | 7.3 8.6 |
| Determine Equivalent Pipe Length from pump dischar | go to soil dispersal area discharge | 60 65 | | 10.0 |
| Determine Equivalent Pipe Length from pump discharge point. Estimate by adding 25% to supply pipe length from pump discharge. | | 70 | | 11.4 |
| (D.2) X 1.25 = Equivalent Pipe Length | | 75 | (A) (1.484) (3.8) (4.40) (8.) (3.) (4.) | 13.0 |
| | | 85 | | 16.4 |
| 80 ft X 1.25 = | 100.0 ft | 95 | | 20.1 |
| G. Calculate Supply Friction Loss by multiplying Friction | Loss Per 100ft (Line E) by the Equivo | alent Pipe Length (Li | ne F) and divide by 100. | |
| Supply Friction Loss = | , , , , , , | | | |
| 2.23 ft per 100ft X | 100.0 ft ÷ 100 | = 2.2 | T _{ft} | |
| Z.25 It per foote X | 100.0 | | | |
| 1. Total Head requirement is the sum of the Elevation D | Difference (Line A), the Distribution F | lead Loss (Line B), Ad | ditional Head Loss (Line C), | and the Supr |
| Friction Loss (Line G) | .,, | (= | , " | |
| | | | 242 | |
| 17.0 ft + 5.0 ft | +ft + | 2.2 ft = | 24.2 ft | |
| . PUMP SELECTION | | | | |
| A pump must be selected to deliver at least | 29.0 GPM (Line 1 or Line 2) wi | th at least | 24.2 feet of to | otal head. |
| Comments: | | | | |
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| • | F | PERCOLA | TION TES | T SHEET | 1 | 1 |
|-------------------------|--------------------------------------|-----------------------------|---|----------------------------|---|---------------------------|
| est hole lo | cation propos | seo site | Hole# | Da | ate test hole was prepared: 1/2 | 1/14_ |
| epth of ho | le bottom: | | _ inches | Diameter of hole | :_ <u>_(e</u> | nes |
| oil Data fr | om test hole: | depth, inches | | soil texture: | soil colo | r |
| ate and ho | our of initial wate | er filling: 2.3 | $\frac{2 \cdot 4}{1 \cdot 4}$ Do not in hole for 4 ho | epth of initial wa | gravel in bottom of hole:ater filling:/2above l | nole bottom |
| ercolation Iaximum v | test conducted b water depth abov | y: Kanoy re hole bottom | ftn de 50 during test: | inche | Percolation test started at | (am (pm) |
| TIME | INTERVAL (MINUTES) | WATER DEPTH | WATER DROP (fraction) | WATER DROP (decimal) | PERC RATE CALCULATION | conversions 1/16 = .06 |
| | start 20 | 8 7 18 | 7/8 | . 88 | $\frac{20}{\text{TIME}} \div \frac{33}{\text{DROP}} = \frac{22.7}{\text{PERC}} \mathbf{A}$ | 1/8 = .13 3/16 = .19 |
| | REFILL 20 | - <u>8</u> - <u>7</u> '8 | 7/8 | 88 | $\frac{20}{\text{TIME}} \cdot \frac{\text{(f)}}{\text{DROP}} = \frac{22.7}{\text{PERC}} \mathbf{B}$ | 1/4 = .25 5/16 = .31 |
| | REFILL 25 | <u>&</u> -7/8 | 11/8 | 1.13 | OS : 1:13 = OO C TIME DROP PERC | 3/8 = .38 7/16 = .44 |
| | REFILL | | | | TIME DROP PERC | 1/2 = .5 |
| | REFILL | | | | TIME DROP PERC | 9/16 = .56 5/8 = .63 |
| | REFILL | | | | TIME DROP PERC (Decimal) | 11/16 = .69 3/4 = .75 |
| | REFILL | | | | TIME DROP PERC (Decimal) | 13/16 = .81 |
| | REFILL | | | | · DROP PERC (Decimal) | 7/8 = .88 15/16 = .94 |
| | | | Ten Percer | nt Calculation | * | |
| A,B,C | | | | B,C,D | | |
| - | of ABC Sma | | ē | | of BCD × 0.10 = | |
| C,D,E | | | | D,E,F | of BCD of DEF Smallest#of DEF | |
| _ | of CDE Sma | | ÞE | Smallest # | of DEF × 0.10 = | |
| E,F,G | of EFG Sma | llest#of EF | | F,G,H | of FGH Smallest # of FGH | |
| Smallest | # of EFG × 0. | 10 = | _ . | Smallest # | of FGH × 0.10 = | |

* If the top number in each set of boxes is larger than the bottom number, take another reading. If the top number is equal to or smaller than bottom number, average the 3 numbers for the perc rate.

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| Home Information | INSPECTION | ON REPO | K1 | | |
| Does the structure contain any of the fol | lowing elements? | | | | |
| Garbage disposer Yes | Dis | hwasher | Yes No | | |
| Grinder pumpYes | Lift | $\frac{1}{2}$ pump in $\frac{1}{2}$ | Yes No | No | . • |
| Garbage disposer Yes Grinder pump Yes Effluent screen installed? Yes | No Eff | luent screen | manufacturer | | |
| Alarm required? Yes No | | | | | |
| Alarm required? YesNo | Alarm Type/ | ECTTI | Alarm manufac | cturer | |
| Lift pump in system?Yes | No Pump manuf | facturer | 29 | | |
| _ | _ | | - Tom | | |
| Number of bedrooms 2 5/3 | ed for 3 | | | | |
| | , | | , | | |
| Component Information | m + 500 lift | | T. Clark | | |
| Component Information Tank size | Tank manufa | acturer | | | |
| Drainfield size 380 5% | , [4 , | | | | |
| Drainfield medium | Madium mo | nufacturar | 10 V 38' | mar | |
| Drainfield medium size/depth | IVICUIUIII IIIAI | nutacturer . | 70 1 30 | mound | |
| · · · · · · · · · · · · · · · · · · · | **** | | | | |
| Soil Verification | | | | | |
| Vertical separation verified for | Boring #1 on | Dej | oth <u>+36</u> | | |
| Martial garantian value 1 Co. | D 10 | _ | | | |
| Vertical separation verified for | Boring #2 on | De _l | oth | | |
| Vertical separation verified for | Boring #3 on | De _l | oth | | , |
| • | | | | | |
| Setback Verification | | | | · | |
| | TANK | DRAI | NFIELD | • | |
| Distance to Well | +100 | • | +100 | | |
| Distance to Building | +10 | *************************************** | +20 | | |
| Distance to Property Line Distance to OHWof Lake | +10 | | +10 | | |
| Distance to OHW of Lake Distance to Pressure Line | Company Compan | | , | | |
| Distance to Pressure Line Distance to Wetland/Protected | Water + 10-0 | *************************************** | T100 | | |
| Distance to Wetland/Trotected | water <u>'75</u> | | 100' | | • |
| . / , | / | 1 | | $\mathcal{A} \cap \mathcal{A}$ | 0/00 |
| Date System Installed $\frac{10}{5}$ | 15 Installer M | aanun (| only Inspector _ | fantt J | toll |
| /-/- | | 1 | This pector of | | · · · · · · · · · · · · · · · · · · · |
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| | CERTIFICATE (| OF COMP | LIANCE | | |
| () Certificate Is Hereby Denied | • | | · | | |
| (X) Certificate is Hereby Granted Base | ed upon the Application | addendum | from plane appoint | ions and all -4b | aumnortina deta |
| With property maintenance, this system | can be expected to function | n satisfacto | uoiii, piaiis, specillicat | ions and an other | supporting data. |
| Y.O.Chia | | . , | | a guarantec. | // |
| fant to tall | | 175 12 | spector | 10, | 15/15 |
| Signature | Titl | le | | Date | |
| (Certificate of Compliance is not valid u | nless signed by a Register | ed Qualified | d Employee) | | |
| | • | | | | |

Becker County Planning & Zoning 835 Lake Ave, P O Box 787 Detroit Lakes, MN 56502-0787 Phone (218)-846-7314; Fax (218)-846-726

OCT 1 9 2006 Phone (218)-846-7314; Fax (218)-846-7266 Onsite Septic System Site Evaluation/Design (if parcel is a new split and a parcel number has not yet been issued, indicate the main parcel number from which the new parcel has been split from) Section 13 Township 139 Range 40 Township Name Erie Lake Classification Legal Description: SY2 of SE 14 Project Address: 34454 190th St Detroit Lakes, MN 56501 PROPERTY OWNER INFORMATION (as it appears on the tax statement, purchase agreement or deed). Owner's First Name Grant E: Brenda L. Owner's Last Name Graham Mailing Address 34454 190 th St. City, State, Zip Detroit Lakes MN 570501 Phone Number 847 - 1254 DESIGNER/INSTALLER INFORMATION Designer Name Dale J. Kenner Company Name D+B Septic+Landscape License # 2591

Address 3/664 St. Hwy 34 D. L. Phone Number 218-841-3781

218-841-3781 Installer Name OWNER Company Name Phone Number Address

4. SYSTEM DESIGN INFORMATION

Date of Site Evaluation 10/13/06

EXISTING SYSTEM STATUS - Check One

No existing system-new structure
Cesspool/Seepage
Failing (other than cesspool)
Undersized
Replacement or repair to existing

Design Flow 300 Gallons Per Day Number of Bedrooms 2
Garbage Disposal Yes X No Grinder Pump in House Yes No Lift station in House Yes No

What will new system serve? Check one

Dwelling
Resort/Commercial
Commercial (non resort)
Other – explain below

Well Depth 200
Depth of other wells within 100 ft of system

Depth to Restricting Layer

Maximum Depth of System

Original Soil Compacted Soil

Type of Soil Observation

Probe Boring

Depth to Restricting Layer

Maximum Depth of System

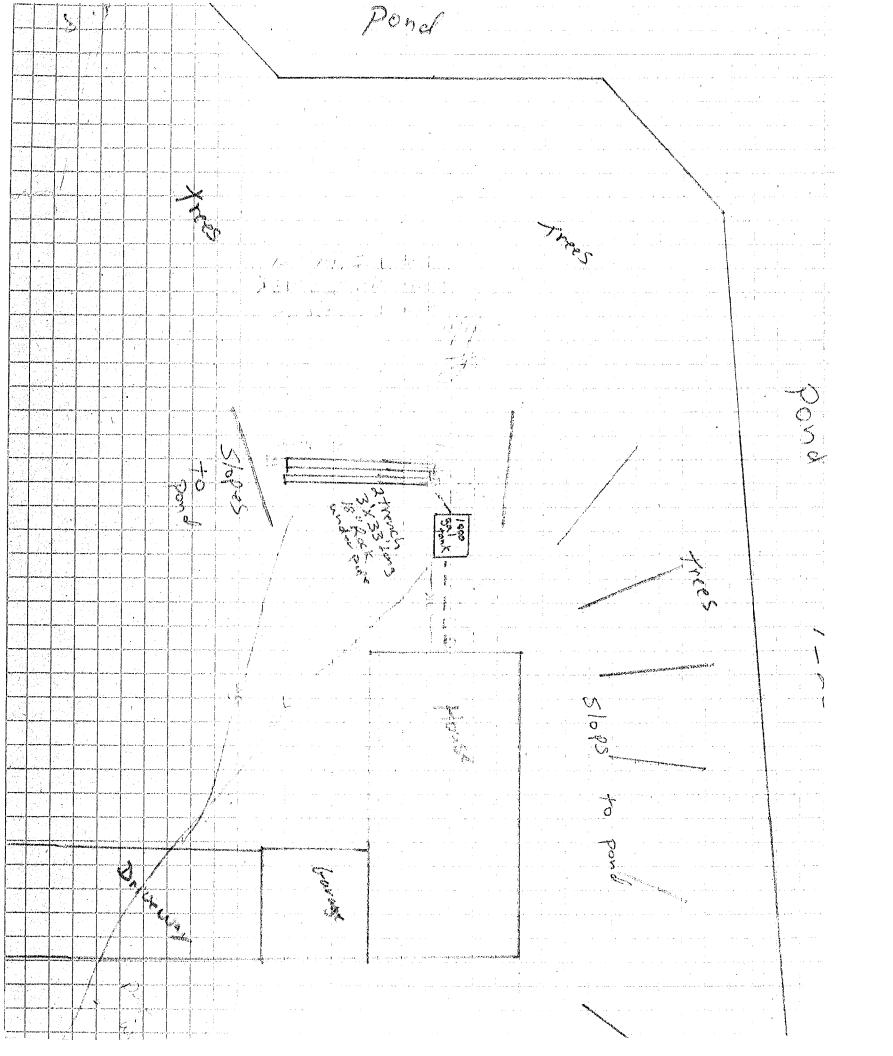
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| gal H | eptic Tank ift Station olding Tank ther Tanks | | Type of Drainfiel to be used Chamber H10 Drainfield J8* Ro Gravelless Experimen No Drainfi | EQ3 Rock ock Depth | | Size of Lift Pu | n Imp ne | |
|--|--|--|--|--|--|--|--|--|
| Trence At-gray | ade ure Bed age Bed ad | <u>300</u> | sq ft sq ft sq ft sq ft | | Distance to Well Distance to Build Distance to Propositance to OHW Distance to Press | ling // erty Line // / ure Line // |) | RAINFIELD 146 30 200 F 88 88 |
| | | Soil Sizing | | | | other than .83, a | | |
| Depth G-8" | Texture top soil | Color loyr/2/ | Structure | 100 CO 10 | Depth 50 - 71 " | Sand Joan | Color | Structure |
| 8-24" | Sand | 10yr 4/2 | | | 78-184" | 20 40 | 3/3 10/2 | |
| 24-38" | 11 60 | 10 yr 3/6 | | | | | | |
| 38-50" | le u | 10 yr 4/6 | | | | | | |
| I. ED Alu | e t. K | enner | certify that I ha | ive comple | ted the precedin | g design work | | vith all |
| | me of Designer) equirements (incommon ance). | | limited to Minnes | ota Chapte | r 7080 and the | Becker County | Individual Sev | vage Treatment |
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